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In The United States Patent And Trademark Office

In Re Application: Tianqing He et al.

Filing Date: 11/15/03

Examiner: Jiping Lu

Serial No: 10/714,471

Art Unit: 3749

Invention: Device And Method For Rapid Drying Of Porous Materials

## **AFFIDAVIT**

NOW COMES the undersigned, who affirms and says:

- My name is Ali Regimand. I am the president of InstroTek, Inc. and a coinventor for the Device and Method for Rapid Drying of Porous Materials filed in the United States Patent Office with Serial #10/714,471.
- 2. The Vacuum Drying Apparatus and Method disclosed and claimed in serial #10/714,471 has been successfully manufactured and marketed as the "CoreDry' by InstroTek, Inc., the company which I am President. The CoreDry is priced at \$4910 per unit and since its marketing launch in 2004, my company has sold a total of 120 units. The volume for this product is expected to quadruple in the next 3 years because of the newly developed ASTM standard, described below, and Department of Transportation Specifications currently being developed in many of the states.
- 3. CoreDry does not have a price advantage over other vacuum dryer models on the market because the CoreDry, to my knowledge, is the only vacuum dryer for porous materials like asphalt currently being sold. The CoreDry has been successful in the market because it represents an advance in the art and has provided the users a fast and more accurate method of testing asphalt samples.
- Attached as Exhibit A is the newly developed American Society for Testing and Materials (ASTM) standard practice, specifically developed for the CoreDry. To my knowledge, there are no other ASTM specifications for other Vacuum Drying Apparatus, since there are no other vacuum devices or processes available for asphalt drying.

ASTM International is one of the largest voluntary standards development organizations in the world for development of technical standards for materials, products, systems, and services. Standards developed at ASTM are the work of over 30,000 ASTM members. These technical experts represent producers, users, consumers, government and academia from over 100 countries.

ASTM standards are accepted worldwide by public and private agencies. In fact, some agencies will not allow the use of an equipment, process or material without an ASTM specification.

Due to the newly developed ASTM standard, CoreDry is now a process that is internationally recognized in the asphalt testing field. This standard further validates CoreDry as a new and useful process for accurate and fast drying of porous asphalt samples.

Attached as Exhibit B are procedures established in Colorado, Pennsylvania and a test report from Colorado regarding the CoreDry. We also know that Florida and Alabama are currently developing specifications for the CoreDry, with others states following close behind. These documents and specifications further independently validate the CoreDry technology and the advance in the art represented by the CoreDry technology and patent application, serial #10/714,471.

THE AFFIANT, first being warned that willful false statement and the like are punishable by fine, imprisonment, or both under Title 28 U.S.C. 1001, states that the above information is true except those things stated on information and belief and as to those things the undersigned believes them to be true.

This the 13th day of September, 2006

An Regimand, President InstroTek, Inc.



Designation: D 7227 - 06

## Standard Practice for Rapid Drying of Compacted Asphalt Specimens Using Vacuum Drying Apparatus<sup>1</sup>

This standard is issued under the fixed designation D 7227; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript apsilon (a) indicates an editorial change since the last revision or reapproval.

### 1. Scope

1.1 This practice covers the process of drying compacted asphalt specimens using vacuum drying apparatus.

1.2 The specimens dried by this practice remain at room temperature, which helps in maintaining specimen integrity during the drying process.

1.3 This practice can be used for compacted cylindrical and cubical bituminous laboratory and field specimens

1.4 This practice can also be used for drying other construction materials such as concrete, soils, aggregates and loose asphalt mixtures. Use manufacturers recommendations for drying other construction materials.

1.5 The values stated in SI units are to be regarded as the standard.

1.6 This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory requirements prior to use.

### 2. Referenced Documents

2.1 ASTM Standards; 2

D 5361 Practice for Sampling Compacted Bituminous Mixtures for Laboratory Testing

## 3. Significance and Use

3.1 Specimen dry weight is a critical measure in determination of accurate density and many other tests in the construction and raw materials industries. Drying specimens at room temperature is required for some tests and provides an advantage for other tests to ensure the integrity and to preserve the characteristics of specimens.

3.2 This practice covers drying compacted asphalt specimens in a vacuum chamber that is capable of keeping the specimen at close to room temperature. A vacuum pump reduces the pressure inside the chamber, thus allowing water to evaporate at low temperature. Since the specimen naturally cools during the evaporation process, making water harder to evaporate, it is important to have proper temperature controls in the chamber to ensure specimen remains at close to room temperature. Automatic controls within the unit allow the specimen to remain at close to room temperature by periodically allowing a flow of warm air to enter the vacuum chamber. Cycling between vacuum and airflow conditions allows the specimen to dry in a short period of time. Completely saturated specimens with over 30 g of retained water can be dried in about 30 minutes. For most field cores that are not completely saturated the drying time is generally less than 15 minutes.

Note 1—Cycle time (period) can depend on the material composition. Each cycle involves an alternating period of 30 to 180 seconds of vacuum operation and 30 to 120 seconds of air flow.

- 3.3 This method can be used for 100 mm diameter, 150 mm diameter cylindrical, and cubical compacted bituminous specimens.
- 3.4 This method can also be used for drying loose asphalt mixtures, aggregate samples and other solid specimens. Follow manufacturers recommended procedures for drying specimens other than compacted biniminous specimens.
- 3.5 This method can be used to determine moisture content and amount of water loss during drying by weighing the sample before and after the drying operations.

#### 4. Apparatus

4.1 Absorptive cloth or paper towels, for drying water from surface of the specimens.

4.2 Vacuum Chamber, with a pump capable of evacuating a sealed and enclosed chamber to a pressure of 6 mm Hg, when at sea level. The chamber shall be large enough to accommodate specimens of 150 mm width or diameter and 180 mm in height. The device shall have an automatic vacuum, airflow and temperature control features to ensure proper drying of the specimen at close to room temperatures. Automatic controls of

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This practice is under the jurisdiction of A3TM Committee D04 on Road and Paving Materials and is the direct responsibility of Subcommittee D04.21 on Specific Gravity and Dentity of Biuminous Mixtures.

Current addition approved Feb. 13, 2006. Published March 2006.

For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For Annual Book of ASTM Standards volume information, refer to the standard's Document Summary page on the ASTM website.

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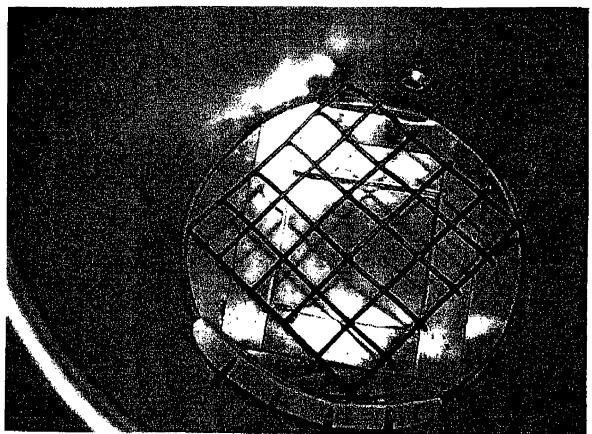


FIG. 1 Water Removal Plate and Sample Holder Installed in Sample Chamber

the unit shall be calibrated by the manufacturer prior to initial use. The device shall have the capability to display vacuum readings in the chamber and number of cycles.

4.3 Water Removable Plate, used for removing free water from the bottom surface of the specimen chamber.

4.4 Blectronic cold trap with an airflow divider plate, used for trapping water and stopping it from entering the vacuum pump.

4.5 A handheld infrared temperature sensor accurate to ±5°C for measuring surface temperature of the specimens.

#### Sampling

5.1 Test specimens may be molded from laboratory prepared specimens or taken from the pavement in the field. Field specimens should be obtained in accordance with Practice D 5361.

## 6. Test Specimen

- 6.1 To speed up the drying process, keep and maintain the specimens to be dried between 15 °C and 30°C.
- 6.2 If desired, specimens may be separated from other pavement layers in accordance with D 5361.

#### 7. Procedure

7.1 Turn On the Unit:

Plug the unit in a power outlet and turn on the on/off switch. Follow manufacturers recommendations for warm up and self test procedures.

- 7.2 Daily Test: Everyday before starting the testing operation, dry the cold trap and the specimen chamber. Run the unit without any specimens. The pressure reading on the display should be 6 mm Hg. or less. If the indicated pressure is higher than 6 mm. Hg. check the system for items that might need service, such as oil level and quality, seals, or water in the chamber. Refer to the manufacturer's trouble shooting instructions for obtaining a proper pressure reading in the chamber. For drying other construction materials, follow manufacturer's recommendations for pressure requirements in the chamber.
- 7.3 Drying Specimens: Use a handheld infrared thermometer to ensure that the surface temperature of the specimen is between 15°C and 30°C. If the specimen is below 15°C or above 30°C, place the specimens in a room temperature environment until the surface temperature approaches the required testing temperature of 15°C to 30°C.
- 7.3.1 Use paper towel or an absorptive cloth to remove any standing water from the surface of the specimen.
- 7.3.2 Place the specimen on top of the specimen support plate inside the chamber.

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7.3.3 Place the lid on the vacuum chamber and press the lid down to ensure secure contact between the lid and the chamber. Press the appropriate key, for example the Start key, to begin the drying process.

7,3.4 When the specimen is dry, the unit will automatically stop. The unit is calibrated at the factory to sense a "dry specimen condition". Dry specimen condition is determined at the factory for the pressure at which no water remains in the chamber. During testing, the unit continuously reads the pressure inside the chamber and checks this pressure against the "dry specimen condition" pressure determined during factory calibration. Follow manufacturer's procedure for calibrating the device to dry specimen condition.

Note 2—Sample is considered dry when the measured weight after vacuum drying process is 0.2 grams or less of 24-hour oven drying at

7.4 Electronic Cold Trap: Liquid and ice, or both, will accumulate in the cold trap as specimens are drying. Between drying specimens and for faster drying, it is best to remove the cold trap lid and the airflow divider plate and wipe out any free standing water in the cold trap. Always place the divider back into the cold trap before drying the next specimen.

### 8. Report

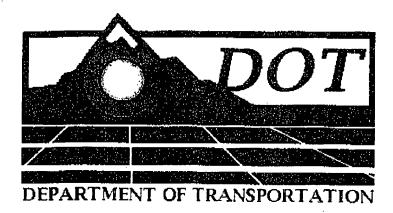
- 8.1 Report the following information:
- 8.1.1 At the end of the drying process, report the ending pressure in run Hg, to the nearest 0.1 mm Hg, and total number of cycles displayed on the screen. This information may be used by the manufacturer or the user for trouble shooting the device, if needed.

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This standard is subject to revision at any time by the responsible technical committee and must be reviewed every five years and if not revised, either responsed or withdrawn. Your comments are invited either for revision of this standard or for additional standards and should be addressed to ASTM International Headquarters. Your comments will receive careful consideration at a meeting of the responsible technical committee, which you may attend, if you teel that your comments have not received a fair hearing you should make your views known to the ASTM Committee on Standards, at the address shown below.

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# Review and Research of Instrotek's "CoreDry®" Report



Neal Retzer
CDOT Materials & Geotechnical Brach
4201 East Arkansas Avenue
Denver, Colorado 80222

## PROBLEM TITLE

Using the CoreDry® to rapidly dry field cores for obtaining bulk specific gravity values:

## PROPOSED WORK PLAN

Problem Statement - Colorado DOT currently oven dries field cores for obtaining bulk specific gravity values. This method is both slow and destructive to the cores. Cores can take up to 24 hours to dry before the dry weight of the core can be taken for the Gsb (Bulk Specific Gravity) calculation. In order to properly dry cores according to CP 44 (modified AASHTO T 166), Method B, cores must be placed in an oven at 230° F and broken down, essentially destroying the core so immersed wet and surface dry weights can no longer be taken.

The CoreDry® offers two advantages over the conventional oven drying method. First, the CoreDry® only takes 15 minutes to dry a core. The current procedure calls for a minimum of 5 hours and as much as 24 hours. Gsb values are often not available the same day a core arrives in the laboratory and project personnel usually must wait overnight for test results. Secondly, the CoreDry® does not destroy the cores. This means the surface dry and submersed weights can be rerecorded if a mistake was made in this process. The cores can also be tested by multiple laboratories if there is a testing dispute.

- 1. Research Objectives The primary objective of this research is to simply evaluate if the CoreDry® compares well enough with the conventional oven dry method for use on projects.
- 2. Research Plan The following steps will be taken to accomplish the objectives of the study.
  - A. Review literature including manufacturer's data as well as other sources that have used or researched the product.
  - B. Conduct testing on cores using both methods and record the results.
  - C. Analyze data and write report.

- D. Present to MAC for approval, rejection or more investigation.
- 3. Research Plan In order to meet the objectives of this research extensive testing must be conducted on numerous cores. One constraint on the research is the amount of time we have to do the testing. The CoreDry® device we are using to conduct the research is on loan from Instrotek and needs to be returned before November 2005. Regions 3 and 5 have volunteered to conduct the testing on project cores and if time permits the central lab will also conduct testing on cores in the lab.

There is not a set amount of cores that will be tested. As many cores as possible will be tested before the CoreDry® must be returned. There are also no parameters on the cores such as aggregate grade, binder grade etc. Both 4-inch and 6-inch cores will be included in the study.

After all of the results are recorded the Gsb of both procedures will be compared for statistical analysis. Any sort of bias in either method will also be investigated.

4. Implementation — If the results in this research are found to be favorable this may be accepted as an approved product and an alternative procedure to the conventional oven drying method. An alternative procedure in CP 44 will also be drafted.

## LITERATURE REVIEW

The CoreDry® apparatus is currently only a couple years old. As a result there has not been very much research conducted on the device and there is not very much literature available for review. Other than the manufacturer's product information there has not been anything published by any transportation agency on the CoreDry®.

Joyce Stone of the Indiana DOT conducted research in the spring of 2005 on the device and was trying to publish the findings in the fall of 2005 in the Transportation Research Board Journal. Her findings are somewhat promising for the CoreDry® but her research did reveal a couple potential problems with the CoreDry®. In a draft report she stated "BSG results using the vacuum method were more consistent and generally higher than those using the standard oven drying method." According to her findings the CoreDry® is precise but not necessarily accurate. Last word is that the research has been dropped and will not be published any time soon.

The Maryland Department of Highways conducted a brief unpublished study comparing the CoreDry® to a fan dry method. It appears as though the fan dry method consists of the cores sitting in front of a fan for at least 8 hours. The CoreDry® outperformed the fan method in their study.

## TESTING PARAMETERS AND CONSIDERATIONS

For proper and accurate testing as well as evaluation of test results some basic parameters need to be considered and or assumed.

For this study field cores used on projects will be tested. The cores density will first be determined by the CoreDry® method and then by the conventional oven dry method. The CoreDry® method must always be done first since the oven dry method destroys the cores. As a result of this always being the case a bias is anticipated in the results. The CoreDry® will dry most of the water out of and off of the core initially. The oven will then dry the remaining water. This may cause a bias in the results by allowing one method to "pretreat" all the cores for the next method it is being compared to. The bias occurs because the oven dry cores have already been dried once by the CoreDry®. The cores will likely not take on much more water for the oven dry method especially if they were already bulked before the CoreDry® dried them out the first time. This pretreating could mean that the cores can only become more dry than they were before making it seem as though the oven dry cores are always less dense than they were before when taking the dry weight.

TEST RESULTS
A summary of the test results are below in Table 1.

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Table 1 (Co	(Conti	ntinued): Summary of Results	mary of Re	sults						
Core #	Size	Thickness	CoreCity Bulk SPG	CP-44 Bulk spG	Bulk SpG Difference	CoreDry Dry Wt. (g)	CP-44 Dry WL (g)	CoreDry Density (%)	CP-44 Density (%)	Density Difference (%)
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14851-19	9		2.198	2.36	0.02	2215.5	2030.7	88.7	88.7	0
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Table 1 (Continued): Summary of Results

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4         178°         225°         2006         3636         802 / 45         40         225           4         178°         222°         20°         779.7         778.2         92.7         52.3           4         2         222°         20°         779.7         778.2         95.7         52.3           4         2         226°         227°         30°         75.3         76.2         92.7         52.3           4         2         226°         227°         30°         76.2         76.2         92.2         52.2           4         2         222°         227°         30°         76.2         76.5         92.2         92.2           4         2         222°         227°         30°         76.2         76.5         76.5         92.2         65.2           4         7         222°         226°         30.0         76.7         76.7         92.9         34.7           6         7.8°         222°         226°         30.0         176.7         76.7         92.9         34.7           6         1.8°         2.8°         2.2°         30.0         176.6         176.4         94.5 </td <td>14376-6</td> <td><del>-1</del></td> <td></td> <td>7.320</td> <td>2.5.1</td> <td>4.0.3</td> <td>0.470</td> <td>3,776</td> <td>3</td> <td>, ,</td> <td>0</td>	14376-6	<del>-1</del>		7.320	2.5.1	4.0.3	0.470	3,776	3	, ,	0
4         17.8°         2222         222         6.0°2         769.8         *Un.6         93.4         52.9         6.2         6.2         6.0°2         775.7         *78.7         94.8         52.2         6.0°2         775.7         *78.2         95.7         55.2         6.0°2         775.7         *78.2         94.8         54.2         6.2         775.7         *78.2         94.8         54.2         6.2         775.7         *78.2         94.8         54.2         6.2         775.7         *78.2         94.8         54.2         6.2         775.7         *77.9         775.4         92.2         52.2         6.2         775.7         775.1         94.5         52.2 <td>14974-7</td> <td>~1</td> <td></td> <td>3.250</td> <td>\$202</td> <td>0.005</td> <td>3C3.6</td> <td>305</td> <td><u>.</u></td> <td>3.42</td> <td>20</td>	14974-7	~1		3.250	\$202	0.005	3C3.6	305	<u>.</u>	3.42	20
4         1787         2222         222         902         7638         70.6         95.5         52.2           4         2         2287         2.275         90.2         773.7         778.2         95.7         55.2           4         2         2266         2.269         30.3         745.8         747.9         948         54.2           7         4         2         2227         2213         0.003         783.6         762.4         92.2         55.2           7         4         17.8         2259         2243         0.01         762.9         701.5         945         55.2           7         4         17.8         2259         2269         0.01         762.9         701.5         945         55.2           7         4         17.8         2259         2269         0.02         77.6         76.3         94.5         56.3           6         17.8         2.26         2.06         17.8         164.4         91.9         51.8           6         1.8         2.26         2.06         16.6         16.6         91.9         51.8           6         1.5         2.26         2.00									1	-	7.5
4         2         2.297         2.275         0.0°2         779.7         778.2         95.7         55.2           4         2         2.266         2.223         0.0°3         743.8         747.9         94.8         54.2           4         2         2.256         2.223         0.0°3         743.6         792.4         91.2         55.2           7         4         1.78         2.259         2.243         0.0°4         76.7         76.7         94.5         55.2           7         4         1.78         2.259         2.243         0.0°4         76.7         76.1         94.5         55.2           6         1.78         2.259         2.273         0.0°4         76.7         775.1         91.9         54.4           6         1.78         2.256         2.275         0.0°3         166.7         175.6         91.9         56.2           6         1.78         2.26         0.0°3         166.7         175.6         91.9         56.2           6         2.26         2.26         0.0°3         166.7         175.6         91.5         55.2           7         1.78         2.26         2.26	14914		17.8	2232	222	9.072	763.8	97.0	3776	277	. U
4         2         2.266         2.253         3.0°3         745.8         747.9         94.8         54.2           4         2         2.227         2.213         0.009         783.6         792.4         92.2         52.5           7         4         17.8°         2.259         2.243         0.0°1         767.3         766.5         94.5         55.5           7         4         17.8°         2.259         2.229         0.0°1         776.7         775.1         95.9         56.3           6         7.78°         2.259         2.275         0.0°3         18.47         16.44         91.9         34.7           6         7.78°         2.250         2.275         0.0°3         18.47         16.44         91.9         34.5           6         7.78°         2.250         2.275         0.0°3         18.47         16.44         91.9         34.5           6         1.38°         2.26         2.275         0.0°3         16.68         173.3         93.5         35.2           7         1.78°         2.36         2.26         0.0°3         14.64         94.5         35.2           8         1.78°         <	14G1457		٨	2.237	2.275	0.0.5	7.9.7	7.82	- i	7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.	., o
4         Z         2.227         2.213         0.009         783.6         792.4         92.2         52.5           7         4         17.8         2.229         2.243         0.016         762.9         701.5         94.5         52.5           7         4         17.8         2.259         2.243         0.01         767.3         766.3         96.2         56.3           7         4         17.8         2.259         2.243         0.01         767.3         775.1         95.9         56.4           6         1.78         2.256         2.256         0.02         1.657.3         1646.4         91.9         34.7           6         2.78         2.256         2.061         1756.5         1734.3         92.5         34.7           6         2.78         2.26         0.061         1756.5         1756.3         93.5         35.2           6         1.78         2.37         0.001         1756.9         1726.9         94.5         35.2           6         1.78         2.37         0.001         1756.9         1726.9         94.5         35.2           6         2.         2.         2.         2. <td>34514.52</td> <td></td> <td>۲.</td> <td>2.256</td> <td>5253</td> <td>3.073</td> <td>745.8</td> <td>5.5.</td> <td><u>8</u></td> <td>3.1</td> <td>in</td>	34514.52		۲.	2.256	5253	3.073	745.8	5.5.	<u>8</u>	3.1	in
7         4         17.8°         2259         2243         3.0°6         7029         7015         945         552           7         4         17.8°         2259         2243         3.0°6         76.7         76.7         76.5         96.2         55.7           7         4         2         2259         2279         0.0°2         776.7         775.1         95.9         56.3           6         1.78°         2.256         2.256         6.003         1847         164.4         91.9         34.7           6         2         3.8°         2.256         2.257         0.061         1785.5         1734.3         91.9         34.5           6         1.32°         2.266         2.267         0.061         1785.5         1734.3         91.9         35.2           6         1.32°         2.264         2.265         0.001         1750.9         1726.9         94.5         35.2           6         1.78°         2.37°         2.265         0.001         1750.9         1726.9         94.5         35.2           6         2         2.264         2.265         0.001         1750.9         1726.9         94.5 <t< td=""><td>14513.17</td><td>İ</td><td>2.</td><td>7.27</td><td>2.273</td><td>0.003</td><td>75.3.6</td><td>÷ 25.</td><td>92.2</td><td>85 10 10 10 10 10 10 10 10 10 10 10 10 10</td><td>7</td></t<>	14513.17	İ	2.	7.27	2.273	0.003	75.3.6	÷ 25.	92.2	85 10 10 10 10 10 10 10 10 10 10 10 10 10	7
6         1 778*         2.254         2.254         0.0*1         7673         7665         96.2         56.7           6         2         2.254         2.275         0.0*2         776.7         775.1         95.9         56.4           6         2         2.258         2.275         0.003         1889         1844         91.9         34.7           6         2         38*2         2.256         2.256         0.061         1785.5         1744.4         91.9         31.8           6         2         38*2         2.256         0.061         1785.5         1744.4         91.9         31.8           6         1 32*         2.264         2.265         0.061         1786.9         1667.5         94.5         35.2           6         1 78*         2.37*         0.001         1750.9         1726.9         94.5         35.2           6         1 78*         2.37*         0.001         1750.9         1726.9         94.5         35.2           6         2         2.264         2.265         0.001         1750.9         1726.9         94.5         35.2           6         2         2.264         2.261	255.5		*8.7	2.954	2,243	30.6	702.9	70:5	5.82	13 13 13 13 13 13 13 13 13 13 13 14 14 14 14 14 14 14 14 14 14 14 14 14	ان.
4         2         2.251         2.273         0.0*2         775.1         95.9         56.4           6         1.78*         2.256         2.256         2.256         3.063         1669         1662         94.5         34.7           6         2         38*         2.256         2.256         3.061         1785.6         1734.3         91.9         31.2           6         2         2.266         2.257         0.061         1785.6         1734.3         93.0         30.5           6         1 32*         2.264         2.252         0.081         1585.4         94.5         35.2           6         1 38*         2.376         2.265         0.001         1750.9         1726.9         94.5         35.2           6         1 78*         2.376         2.265         0.001         1750.9         1726.9         95.3         35.2           6         2*         2.264         2.221         0.083         164.6         1841.5         93.4         35.2           6         2*         2.264         2.221         0.083         164.6         1841.5         93.4         35.2           6         2*         2.264	201		o o	2.25	E50.5	9.00	757.3	756.3	95.2	15 15 15 15 15 15 15 15 15 15 15 15 15 1	0
6         1.78°         2.29°         2.22°         6.003         1889         1844         91.9         34.7           6         2.8°         2.22°         2.22°         6.003         18.7         1844         91.9         31.5           6         2         2.25°         2.25°         6.006         178.5         1734.3         92.5         36.5           6         1.82°         2.264         2.25°         6.006         1168.9         1507.5         93.4         35.7           6         1.78°         2.26°         2.26°         6.001         1750.5         1734.5         93.4         35.2           6         2°         2.37°         2.31°         0.001         1750.5         1724.5         93.4         35.2           6         2°         2.264         2.261         0.003         1646.8         1944.5         93.4         35.2           8         1.78°         2.37°         2.261         0.003         1646.8         1944.5         93.4         35.2           9         2         2.264         2.261         0.003         1646.8         1944.5         93.4         35.2           9         2         2.264	145147 145147		7	122	2.273	9.0.5	7.6.7	775.1	97.9	F 900	o o
6         17.8°         2.296         2.269         6.003         1569.9         1562.2         94.5         34.7           6         2.8°         2.226         2.226         3.003         18-7         1644.4         91.9         31.5           6         2         2.266         2.257         3.061         1785.5         1734.3         92.0         30.5         30.5           6         1 34.°         2.264         2.262         6.001         1786.4         1454.4         94.5         34.2           6         1 78°         2.376         2.265         6.001         1750.9         1726.9         95.3         35.2           6         2         2.264         2.221         0.001         1750.9         1726.9         95.3         35.2           6         2         2.264         2.221         0.003         1646.8         1846.8         1846.8         33.4         35.2           8         2         2.264         2.221         0.003         1646.8         1846.8         1846.8         33.4         35.2	1 2	•									
6         7.78°         2.23°         2.22°         5.00°         1.53°         1.544         91.9         31.8           6         2         2.26°         2.22°         6.003         18-7         1544         91.9         31.8           6         2         2.26°         2.26°         6.001         178.5         1743         91.9         31.8           6         1.82°         2.264         2.26°         0.001         146.4         94.5         33.2           6         1.78°         2.37°         2.30°         0.001         1750.9         1726         94.5         35.2           6         1.78°         2.37°         2.30°         0.001         1750.9         1726         95.3         35.2           7         2.264         2.261         0.003         1546.8         1846.8         1846.8         93.4         35.2           8         2         2.264         2.221         0.003         1546.8         1846.8         1846.8         33.4         35.2					2000	600 6	20321	63231	: B	7.7	30
6         2         3226         2225         6.003         1847         1543         31.8	1:67	ው	8:3	4.22b	5.32.2	COO.S.	1503.5	1	0	a lin	0.1
6         Z         2256         2257         0.061         17855         17443         950         30.0           6         132*         2264         2252         0.062         15089         15075         93.4         35.2           6         138*         228         2265         0.001         1466.4         1494.4         94.5         34.2           6         178*         23°0         23°0         0.001         1750.9         1720.9         95.2         35.2           6         2*         2.254         2.221         0.093         1846.6         1846.5         93.4         35.2           Average         0.064         3.46.8         3.46.8         33.2         35.2	3- 1976	9	<b>8</b> . 3	2.226	2.223	3.063		77.77	5.15	i	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \
6         132*         2254         2252         6.002         1508.5         1507.5         93.4         50.2           6         158*         228*         226.5         6.001         1456.4         1454.4         94.5         54.2           6         178*         23°         23°         6.001         1750.9         1720.9         95.3         55.2           6         2*         2.254         2.221         0.093         1546.8         1846.5         93.4         55.2           Average         0.064         3         3         3         3         3         3	1:67	ō	27	2.256	2.283	9.0e1	1735.5	5.45.5	C:75	) (C) (C) (C) (C) (C) (C) (C) (C) (C) (C	26
6         17.8°         2.28°         2.28°         0.001         1495.4         1454.4         94.3         54.4           6         17.8°         2.3°         2.3°         0.001         1750.9         1720.9         95.3         35.2           6         2°         2.254         2.2°         0.003         1846.8         1846.8         93.4         35.2           Average         0.064         3.064         3.406.3         3.406.3         3.406.3         3.406.3	1.57. 4	9	13.54	2.264	2.252	6.082	15[08.9	1567.3	3.5	3	5 5
6         27         2.35         2.35         0.001         1750.9         1720.9         95.3         55.2           6         2*         2.264         2.261         0.003         1646.8         1846.8         1846.8         33.4         55.2           Average         0.064         3.064         3.463.8         3.463.8         3.463.8         3.463.8	1257	'n	158	3.235	2.263	9.061	1456.4	ा हिल्ल	<u>ှ</u>	3.4%	- C
6 2° 2.264 2.281 0.083 (846.8 (844.8 93.4 5.5.4 Average 0.084	1257	,E	1.8.	2.3.6	2333	100.0	17:50.5	17293	£13	3.5.5	
Average 0.064	1:677	i G		2.254	132.7	0.083	16:16.8	1944.5	93.4	753	70
1.064							ſ			3.00035	1
					Ave 35e	0.064				יינסטאר	<u>.</u>

\*Cores on project 14914 were bulked by two different testers for the CoreDry® and the Oven Dry method

## ADDITIONAL TESTING AND RESULTS

After the initial testing was concluded and the results recorded in Table 1, additional testing was needed to examine if the bias is an outcome of the circumstances or if the oven dry method is actually more effective than the CoreDry® method.

The additional research was conducted to try and take out the bias or the advantage the oven dry method has by always going after the CoreDry® method. Twelve samples were put under a vacuum for 90 seconds and saturated with water much like the Moisture Susceptibility test in Colorado Procedure 5109. The weight of the sample was taken before saturation, after saturation and then again after the sample was dried. This determined how effective each method is in removing water from the samples. The two methods were then compared in how efficient they are in removing water as a percentage.

While conducting the extra testing the CoreDry® did not appear to completely dry some of the samples. The weight was noted and the sample was dried again. This may not be anything major since the CoreDry® is not designed to dry vacuum saturated design samples and the apparatus may have been overloaded but it may have to be written into the procedure to check the core for any residual water on the surface and dry the core again if moisture is visible.

Table 2: Results for Extra Testing with the CoreDry®

				CoreDry		
Sample Number	Original Weight (g)	Saturated Weight (g)	Water Added (g)	Dried Weight (g)	Water Removed (g)	Efficency (%)
391-1	1168.6	1183.2	14.6	1159.5	13.7	93.8%
391-2	1168.4	1181.9	13.5	1169.1	12.8	94.8%
391-3	1169.5	1184.1	14.6	1170.5	13.6	93.2%
399-1	1165.6	1176.9	11.3	1167.3	9.6	85.0%
399-2	1165	1176.1	11.1	1166.8	9.3	83.8%
399-3	1165.8	1176.6	10.8	1167.7	8.9	82.4%
400-1	1144.9	1155.6	10.7	1146.7	8.9	83.2%
400-2	1145	1155.9	10.9	1146.7	9.2	84.4%
400-3	1144.8	1154.9	10.1	1146.6	8.3	82.2%
406-1	1155.1	1161.1	6	1155.9	5.2	86.7%
406-2	1154.6	1160.3	5.7	1155.4	4.9	86.0%
406-3	1154.2	1163.4	9.2.	1155.3	8.1	88.0%

Average

86.9%

Table 3: Results for Extra Testing with the Oven

				Oven Dry				
Sample Number	Original Welght (g)	Pan Tare (g)	Saturated Weight (g)	Water Added (g)	Pan+ Sample (g)	Dried Welght (g)	Water Removed (g)	Efficency (%)
004.4	4469.6	249.3	1183.4	14.8	1419.1	1169.8	13.6	91.9%
391-1	1168.6 1168.4	248.4	1182.2	13.8	1418	1169.6	12.6	91.3%
391-2		254.9	1184.6	15.1	1425.7	1170.8	13.8	91.4%
391-3	1169.5	251.9	1177.7	12.1	1418.4	1166.5	11.2	92.6%
399-1	1165.6	254.7	1176.5	11.5	1420.4	1165.7	10.8	93.9%
399-2	1165	244.6	1177.4	11.6	1411.4	1166.8	10.6	91.4%
399-3	1165.8 1144.9	248.7	1157.8	12.9	1394.7	1146	11.8	91.5%
400-1 400-2	1145	252.1	1157.7	12.7	1398.2	1146.1	. 11.6	91.3%
400-3	1144.8	255.1	1155.5	10.7	1401	1145.9	9.6	89.7%
406-1	1155.1	251.4	1161.4	6.3	1407.1	1155.7	5.7	90.5%
406-2	1154.6	256.9	1160.7	6.1	1412.2	1155.3	5.4	88.5%
406-3	1154.2	254.4	1164.2	10	1409.6	1155.2	9	90.0%

Average 91.2%

## RESULTS SUMMARY

When comparing field cores the average difference in density comes out to be 0.17% and never exceeded a difference of 0.6%. The average Bulk Specific Gravity difference is .004 and never exceeded .016. When conducting the extra testing on design samples the CoreDry® removed 86.9% of the water added while the oven removed 91.2%.

The densities between the two methods were plotted below and an "R" squared value was determined to be .9969.

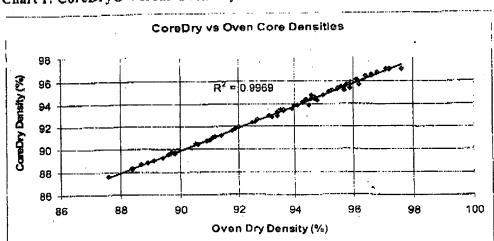


Chart 1: CoreDry® Versus Oven Dry Densities

A  $T_{paired}$  Test was conducted on the densities and showed no statistical difference between the two methods.

t paired = d bar / (Sd /sq rt n)

d bar = 3.76 / 76 = .0495

Sd squared =  $3.76 - (13^2/76) = 1.536$ 

Sd = 1.239

Sq rt n = sq rt 76 = 8.718

t paired = .0495/(1.239/8.718) = .3483

T.05, 76 = 1.668

Since .3483 is less than 1.668, the data strongly suggests there is no difference in densities.

## CONCLUSION

Based on the data analysis it is recommended that the CoreDry® apparatus be accepted as an alternative to the oven dry method (Method B) of CP 44.

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Commonwealth of Pennsylvania Department of Transportation

PA Test Method No. 715LA Revised Feb. 2006 5 Pages

#### Method of Test for

## DETERMINATION OF BULK SPECIFIC GRAVITY OF COMPACTED BITUMINOUS ROADWAY CORE SAMPLES

### 1. SCOPE

1.1 This method of test is intended for determining the bulk specific gravity of bituminous roadway core samples obtained for and governed under the Local Acceptance specification only.

### 2. TEST SPECIMEN

- 2.1 Core samples from the compacted pavement obtained in accordance with PaDOT methods of sampling a compacted roadway.
- 2.2 Specimen size It is recommended, (1) that the diameter of the cored specimen be at least equal to four times the nominal maximum size of the aggregate; and (2) that the thickness of the core be the actual depth of the material as placed on the project or at least 1.5 times the nominal maximum aggregate size.
- 2.3 Specimens shall be free of foreign materials such as seal coat, tack coat foundation material, soil and any other material not a component of the original mix.

## 2.4 Sample Preparation

- 2.4.1 Specimens are to be separated from other pavement layers by sawing or other suitable means. Care shall be exercised to ensure separation does not damage the specimen.
- 2.4.2 Specimens shall be dried to a constant mass (constant mass shall be defined as the mass that is obtained when further drying does not alter the observed mass by more than 0.05 percent) using one of the procedures described:

- (1) Dry the sample for at least 20 hours at  $52 \pm 3^{\circ}$ C ( $125 \pm 5^{\circ}$ F), checking the dry weight at two hour intervals until constant mass is reached.
- (2) Dry the sample in a large, flat pan of known mass in an oven at  $110 \pm 5^{\circ}$ C (230  $\pm$  9°F) until the fine aggregate-asphalt portion can be separated into pieces no larger than 6.4 mm (1/4 in.). Return the sample to the oven, checking the dry weight after cooling to room temperature [25  $\pm$  5°C (77  $\pm$  9°F)], every half hour until constant mass is attained on at least three consecutive weighings. Note: Caution should be exercised before using this method since the sample will be destroyed by this process. Samples coated with paraffin cannot be prepared by this method.
- (3) Dry the sample by exposure to moving air of relatively low humidity while changing the orientation of the sample frequently and checking the dry weight every half hour until constant mass is attained on at least three consecutive weighings.
- (4) Dry the sample in a vacuum drying apparatus meeting the requirements of, and in accordance with, ASTW D-7227-06.

## 2.5 Verification

2.5.1 Use methods 2.4.2(3) and 2.4.2(4) as preparation for acceptance testing only after verification in accordance with the appropriate specification.

## **VOLUMETER METHOD**

### 3. APPARATUS

- 3.1 Weighing Device Conforming to the requirements of AASHTO M-231, Class G2.
- 3.2 Thermostatically controlled water bath designed to maintain the bath temperature at  $25 \pm 0.5$ °C (77  $\pm 0.9$ °F)
- 3.3 Thermometer ASTM 17C (17F), having a range of 19 to 27°C (66 to 80°F), graduated in 0.1°C (0.2°F) subdivivsions
- 3.4 Volumeter Calibrated, 1.2L or an appropriate capacity depending on the sze of the sample.